

Dynamical flexibility of rod and beam systems in transportation

S. Żółkiewski*

Division of Mechatronics and Designing of Technical Systems, Mechanical Engineering Department, Institute of Engineering Processes Automation and Integrated Manufacturing Systems, Silesian University of Technology, ul. Konarskiego 18a, 44-100 Gliwice, Poland

* Corresponding author: E-mail address: slawomir.zolkiewski@polsl.pl

Received 25.02.2008; published in revised form 01.08.2008

Analysis and modelling

ABSTRACT

Purpose: Purpose of this paper is to present a mathematical model of rod and beam systems in transportation. The mathematical model is presented in the form of dynamical flexibility of systems. Systems are considered as flexible rotating rods and flexible rotating beams. In solution there was taken into account the interaction between the main motion and local vibrations of elements.

Design/methodology/approach: The dynamical flexibility was derived by the approximate method, the Galerkin's method. The example dynamical characteristics were presented in form of attenuation-frequency characteristics. The dynamical flexibility was derived on the basis of known equations of motion derived in other publications.

Findings: There can be observed so called the transportation effect. This effect consists in that when analyzed system rotates with some angular velocity in the characteristic of dynamical flexibility we can notice additional poles and after increasing angular velocity it is noticeable that created modes are symmetrically propagated from the original mode. It is also a palpable fact, instead of the original mode there is created zero.

Research limitations/implications: Analyzed systems are simple linear type beams and rods in rotational motion. Motion was restricted to plane motion. Future research ought to consider complex systems, damped models and also nonlinearity.

Practical implications: Practical implications of derived mathematical models of beam and rod systems both the free-free ones and fixed ones is a possibility of derivation of the stability zones of analyzed systems and derivation of eigenfrequencies and zeros in the way of changing the value of angular velocity.

Originality/value: Presented models apply to rotating flexible rod and beam systems with taking into consideration the transportation effect. It is a new approach of analyzing rod and beam systems and can be put to use in modelling and analyzing machines and mechanisms in rotational transportation.

Keywords: Applied mechanics; Numerical techniques; Vibrations; Transportation effect

1. Introduction

There are many technical problems connected with vibrations in contemporary technical sciences and there are many methods of analyzing vibrations. One of the most popular methods is a method of dynamical flexibility. This method can be used both to discrete and continuous systems. Thank to this method we can

very easily assign resonance zones and find the amplitude of vibrations of the analyzed element, find the zeros of dynamical characteristics where the vibrations are minimally.

In this thesis considered problems apply to rotational beam and rod systems. The rotation is treated as transportation movement. In the literature [2-6, 12-13] there are publications connected with the subject area of vibrating systems in transportation as distinguished from ones connected with the

stationary systems [1, 7-11, 14-19]. There are derived mathematical model in form of dynamical flexibility of the system. The dynamical flexibilities were derived on the basis of formerly derived equations of motion.

There are many ways of minimizing amplitudes of vibrations for example in the way of changing forces acting into the systems, changing framework of system or changing the geometrical or physical parameters of the system.

2. Dynamical flexibility of rod systems

In this section there was presented the dynamical flexibilities of rod systems both in form of mathematical model and the dynamical characteristics on the chart (Fig. 1). The equation (1) applies to the dynamical flexibility of stationary free-free system derived by the Galerkin's method.

$$Y(\Omega) = \frac{2}{\rho \cdot A \cdot l} \cdot \sum_{n=0}^{\infty} \frac{\cos(n\pi) \cdot \cos\left(\frac{n\pi x}{l}\right)}{a^2 \cdot \left(\frac{n\pi}{l}\right)^2 - \Omega^2}, \quad (1)$$

where:

$Y(\Omega)$ – the dynamical flexibility in function of frequency of extorted force,

A – the cross-section of rod,

l – length of the rod,

ρ – mass density of the rod,

n – mode of vibrations of rod,

a – velocity of the wave propagation in the rod,

Ω – frequency of vibrations,

x – the position of analyzed section.

The equation (2) presents the dynamical flexibility of the stationary fixed rod.

$$Y(\Omega) = \frac{2}{\rho \cdot A \cdot l} \cdot \sum_{n=0}^{\infty} \frac{\sin\left[\left(n + \frac{1}{2}\right)\pi\right] \cdot \sin\left[\frac{(2n+1)\pi x}{2l}\right]}{a^2 \cdot \left[\frac{(2n+1)\pi}{2l}\right]^2 - \Omega^2}. \quad (2)$$

The equation (3) is a dynamical flexibility of free-free rod system rotating with the angular velocity ω .

$$Y = \sum_{n=0}^{\infty} \frac{2 \cdot \cos(n\pi) \cdot \left(a^2 \cdot n^2 \cdot \frac{\pi^2}{l^2} - \Omega^2 - \omega^2\right) \cdot \cos\left(n\pi \frac{x}{l}\right)}{\rho \cdot A \cdot l \cdot \left[\left(a^2 \cdot n^2 \cdot \frac{\pi^2}{l^2} - \Omega^2 - \omega^2\right)^2 - 4 \cdot \omega^2 \cdot \Omega^2\right]}. \quad (3)$$

The equation (4) is a dynamical flexibility of fixed rod system rotating with the angular velocity ω .

$$Y = \sum_{n=0}^{\infty} \frac{2 \cdot \sin\left(\frac{2n+1}{2}\pi\right) \cdot \left[a^2 \cdot \left(\frac{2n+1}{2}\right)^2 \cdot \frac{\pi^2}{l^2} - \Omega^2 - \omega^2\right] \cdot \sin\left(\frac{2n+1}{2}\pi \frac{x}{l}\right)}{\rho \cdot A \cdot l \cdot \left\{\left[\left(a^2 \cdot \left(\frac{2n+1}{2}\right)^2 \cdot \frac{\pi^2}{l^2} - \Omega^2 - \omega^2\right)\right]^2 - 4 \cdot \omega^2 \cdot \Omega^2\right\}}. \quad (4)$$

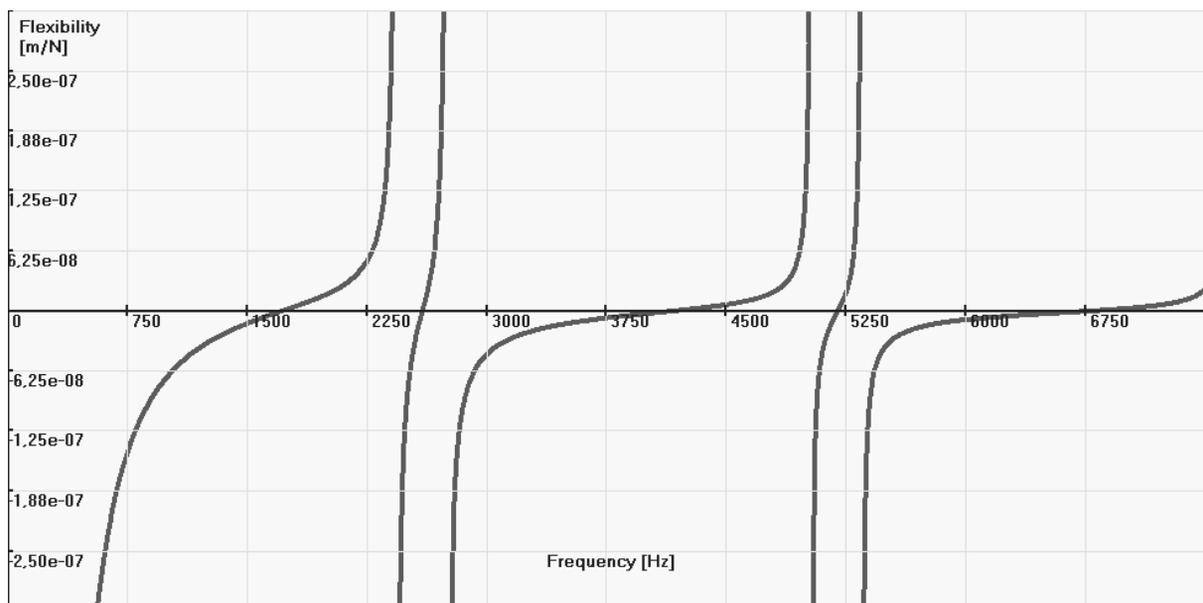


Fig. 1. The dynamical flexibility of free-free rod rotating with angular velocity equals 1000 rad/s

3. Dynamical flexibility of beam systems

This section presents the dynamical flexibilities of beam systems both the stationary ones and in transportation as well. The results are presented as mathematical models of analyzing systems derived by the Galerkin's method and as dynamical characteristics on charts presented onto Figures (Fig. 2 and Fig. 3).

The equation (5) presents dynamical flexibility of free-free stationary beam systems derived on base of known equations of motion of this beam.

$$Y(\Omega) = \frac{1}{\rho \cdot A \cdot \gamma_n^2} \cdot \sum_{n=1}^{\infty} \frac{X(l) \cdot X(x)}{c^2 \cdot \left(\frac{2 \cdot n - 1}{2} \cdot \frac{\pi}{l}\right)^4 - \Omega^2} \quad (5)$$

where:

I_Z – geometric momentum of inertia,
 E – Young modulus,
 c – the formula (6):

$$c = \sqrt{\frac{E \cdot I_Z}{\rho \cdot A}} \quad (6)$$

$$X(x) = \sin(kx) + \frac{\cos(kl) - \cosh(kl)}{\sin(kl) + \sinh(kl)} \cdot \cos(kx) + \sinh(kx) + \frac{\cos(kl) - \cosh(kl)}{\sin(kl) + \sinh(kl)} \cdot \cosh(kx) \quad (7)$$

and

$$k \approx \frac{2 \cdot n + 1}{2 \cdot l} \cdot \pi, \quad n = 0 \Rightarrow k = 0. \quad (8)$$

The equation (8) presents dynamical flexibility of fixed stationary beam systems derived on base of known equations of motion of this beam.

$$Y(\Omega) = \frac{1}{\rho \cdot A \cdot \gamma_n^2} \cdot \left[\frac{X(l) \cdot X(x_{k=0})}{\Omega^2} + \sum_{n=1}^{\infty} \frac{X(l) \cdot X(x)}{c^2 \cdot \left(\frac{2 \cdot n + 1}{2 \cdot l} \cdot \pi\right)^4 - \Omega^2} \right] \quad (9)$$

where:

$$X(x) = \sin(kx) + \frac{\cos(kl) + \cosh(kl)}{\sin(kl) - \sinh(kl)} \cdot \cos(kx) + \quad (10)$$

$$-\sinh(kx) - \frac{\cos(kl) + \cosh(kl)}{\sin(kl) - \sinh(kl)} \cdot \cosh(kx),$$

$$k \approx \frac{2 \cdot n - 1}{2 \cdot l} \cdot \pi. \quad (11)$$

The dynamical flexibility of rotating free-free beam with angular velocity signed as ω with the same $X(x)$ as in the equation (7).

$$Y = \frac{-X(l) \cdot X(x_{k=0}) \cdot (\Omega^2 + \omega^2)}{\rho \cdot A \cdot \gamma_n^2 \cdot (\Omega^2 - \omega^2)^2} + \sum_{n=1}^{\infty} \frac{\left[c^2 \cdot \left(\frac{2 \cdot n + 1}{2 \cdot l} \cdot \pi\right)^4 - \Omega^2 - \omega^2 \right] \cdot X(l) \cdot X(x)}{\rho \cdot A \cdot \gamma_n^2 \cdot \left[\left(c^2 \cdot \left(\frac{2 \cdot n + 1}{2 \cdot l} \cdot \pi\right)^4 - \Omega^2 - \omega^2 \right)^2 - 4 \cdot \omega^2 \cdot \Omega^2 \right]} \quad (12)$$

$$Y = \sum_{n=1}^{\infty} \frac{\left[c^2 \cdot \left(\frac{2 \cdot n - 1}{2} \cdot \frac{\pi}{l}\right)^4 - \Omega^2 - \omega^2 \right] \cdot X(l) \cdot X(x)}{\rho \cdot A \cdot \gamma_n^2 \cdot \left[\left(c^2 \cdot \left(\frac{2 \cdot n - 1}{2} \cdot \frac{\pi}{l}\right)^4 - \Omega^2 - \omega^2 \right)^2 - 4 \cdot \omega^2 \cdot \Omega^2 \right]} \quad (13)$$

where:

$$\gamma_n^2 = \int_0^l X^2(x) dx. \quad (14)$$

In the Figure 2 the dynamical flexibility of the free-free beam rotating with angular velocity equal 100 rad/s was presented.

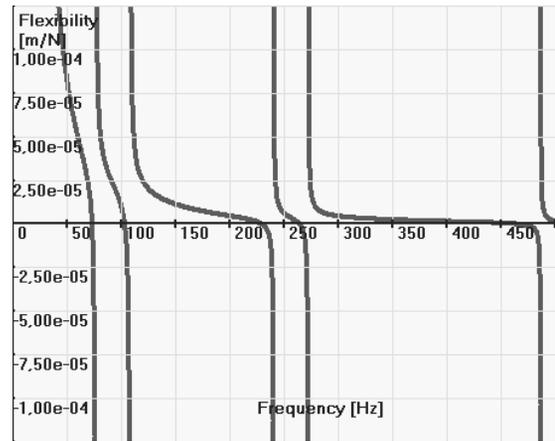


Fig. 2. Dynamical flexibility of the free-free beam system rotating with angular velocity equal 100 rad/s

In the Figure 3 there was presented the dynamical flexibility of fixed beam rotating with angular velocity equal 100 rad/s.

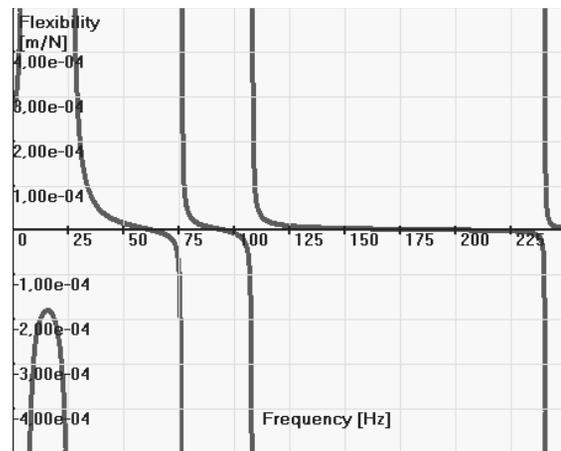


Fig. 3. Dynamical flexibility of the fixed beam system rotating with angular velocity equal 100 rad/s

4. Conclusions

The comfortable method of analyzing vibrations is a method of dynamical flexibility presented in this thesis. The numerical application Modyfit was used to generate the dynamical characteristics shown in this work. Working motion treated here as transportation changes the dynamical characteristics and moves the zeros and modes of dynamical flexibility together with increase of angular velocity both rods and beams. The so called transportation effect has more affect onto beam systems than rod ones.

Acknowledgements

This work has been conducted as a part of research project N 502 071 31/3719 supported by the Ministry of Science and Higher Education in 2006-2009.

References

- [1] J. Awrejcewicz, W.A. Krysko, Vibrations of continuous systems, WNT, Warsaw, 2000 (in Polish).
- [2] A. Buchacz, S. Żółkiewski, Transverse vibrations of the elastic multielement manipulator in terms of plane motion and taking into consideration the transportation effect, Proceedings of the 8th Conference on Dynamical Systems – Theory and Applications, Lodz, 2, 2005, 641-648.
- [3] A. Buchacz, S. Żółkiewski, Formalization of the longitudinally vibrating rod in spatial transportation, International Conference of Machine-Building and Technosphere of the XXI Century, Sevastopol, 4, 2007, 279-283.
- [4] A. Buchacz, S. Żółkiewski, The dynamical flexibility of the transversally vibrating beam in transportation, Folia Scientiarum Universitatis Technicae Resoviensis no. 222, Mechanics b.65 Problems of dynamics of construction. Rzeszow – Bystre, 2005, 29-36.
- [5] A. Buchacz, S. Żółkiewski, Dynamic analysis of the mechanical systems vibrating transversally in transportation, Journal of Achievements in Materials and Manufacturing Engineering 20 (2007) 331-334.
- [6] A. Buchacz, S. Żółkiewski, Mechanical systems vibrating longitudinally with the transportation effect, Journal of Achievements in Materials and Manufacturing Engineering 21/ 1 (2007) 63-66.
- [7] A. Dymarek, The sensitivity as a Criterion of Synthesis of Discrete Vibrating Fixed Mechanical Systems, Journal of Materials Processing Technology 157-158 (2004) 138-143.
- [8] A. Dymarek, T. Dzitkowski, Modelling and Synthesis of Discrete-Continuous Subsystems of Machines with damping, Journal of Materials Processing Technology 164-165 (2005) 1317-1326.
- [9] T. Dzitkowski, Computer Aided Synthesis of Discrete-Continuous Subsystems of Machines with the Assumed Frequency Spectrum Represented by Graphs, Journal of Materials Processing Technology 157-158 (2004) 1317-1326.
- [10] A. Sękala, J. Świder, Hybrid Graphs in Modelling and Analysis of Discrete-Continuous Mechanical Systems, Journal of Materials Processing Technology 164-165 (2005) 1436-1443.
- [11] R. Solecki, J. Szymkiewicz, Rod and superficial systems. Dynamical calculations. Arcades, Building Engineering, Art, Architecture, Warsaw, 1964 (in Polish).
- [12] G. Szefer, Dynamics of elastic bodies undergoing large motions and unilateral contact, Journal of Technical Physics 41/4 (2000) 343-359.
- [13] G. Szefer, Dynamics of elastic bodies in terms of plane frictional motion, Journal of Theoretical and Applied Mechanics 39/ 2 (2001) 395-408.
- [14] J. Świder, G. Wszolek, Analysis of complex mechanical systems based on the block diagrams and the matrix hybrid graphs method, Journal of Materials Processing Technology 157-158 (2004) 250-255.
- [15] J. Świder, P. Michalski, G. Wszolek, Physical and geometrical data acquiring system for vibration analysis software, Journal of Materials Processing Technology 164-165 (2005) 1444-1451.
- [16] S. Woroszył, Examples and tasks of the theory of vibrations, Continuous systems, PWN, Warsaw, 1979 (in Polish).
- [17] G. Wszolek, Modelling of Mechanical Systems Vibrations by Utilization of Graftsim Software, Journal of Materials Processing Technology 164-165 (2005) 1466-1471.
- [18] G. Wszolek, Vibration Analysis of the Excavator Model in GrafSim Program on the Basis of a Block diagram Method, Journal of Materials Processing Technology 157-158 (2004) 268-273.
- [19] K. Żurek, Design of reducing vibration mechatronical systems, Comment Worldwide Congress on Materials and Manufacturing Engineering and Technology, Computer Integrated Manufacturing, Gliwice-Wisla, 2005, 292-297.